

WS 4.1 Capacitance of a cylindrical grid

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This Mathcad 14 worksheet is designed to accompany the author's book "Microwave and RF Vacuum Electronic Power Sources", Cambridge University Press (2018). The section, equation, and figure numbers refer to the corresponding sections, equations, and figures in the book. Data input fields are highlighted in yellow and output fields are highlighted in green.

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This sheet models a section of the grid of width p between the centres of adjacent strips. The grid comprises an array of circular loops surrounded by a uniform dielectric layer and a conducting metal cylinder. The sheet calculates and displays the potential map using a finite difference calculation on a square mesh and calculates the capacitance per unit length of one strip divided by ϵ_0

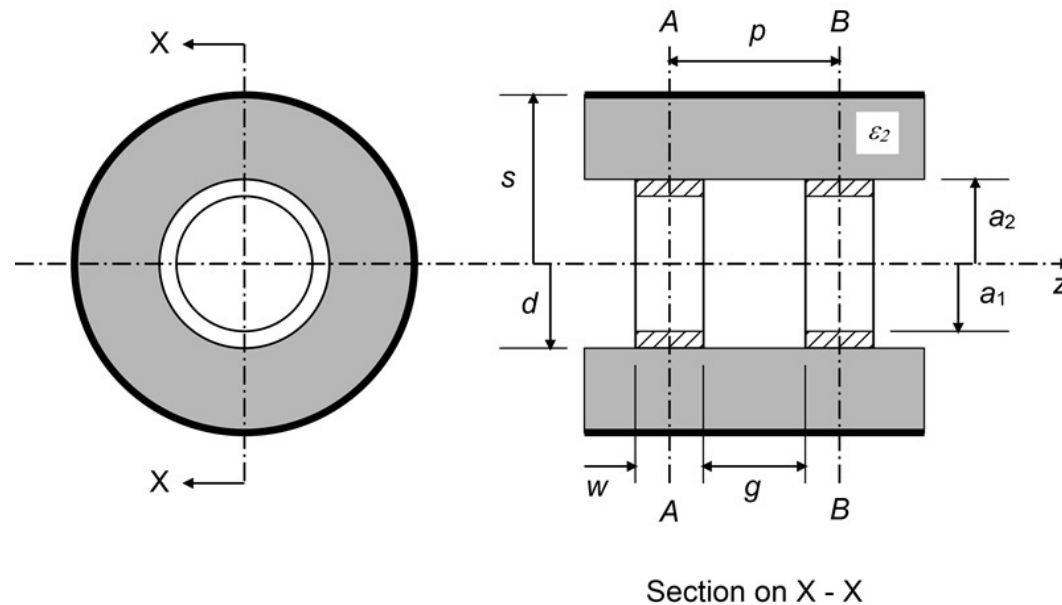


Figure 4.18

Structure dimensions

$$a_1 := 10 \cdot \text{mm} \quad s := 14 \cdot \text{mm} \quad p := 10.0 \cdot \text{mm} \quad w := 8 \cdot \text{mm} \quad t := 1 \cdot \text{mm} \quad \epsilon_r := 2.5 \quad a_2 = a_1 + t$$

Choose mesh size for FD calculations $\text{mesh} := 0.25 \cdot \text{mm}$

$$N_A := \frac{a_1}{\text{mesh}} \quad N_S := \frac{s}{\text{mesh}} \quad N_P := \frac{p}{\text{mesh}} \quad N_W := \frac{w}{\text{mesh}} \quad N_T := \frac{t}{\text{mesh}}$$

$$N_A = 40 \quad N_S = 56 \quad N_P = 40 \quad N_W = 32 \quad N_T = 4 \quad \text{These numbers should be as close to integers as possible}$$

$$N_{A1} := \text{round}(N_A) \quad N_S := \text{round}(N_S) \quad N_P := \text{round}(N_P) \quad N_W := \text{round}(N_W) \quad N_T := \text{round}(N_T) \quad N_{A2} := N_{A1} + N_T \quad N_{W2} := \frac{N_W}{2} \quad N_{P2} := \frac{N_P}{2}$$

$$N_{A1} = 40 \quad N_S = 56 \quad N_P = 40 \quad N_{W2} = 16 \quad N_{A2} = 44 \quad \text{NB: } N_P \text{ and } N_W \text{ must be even numbers}$$

Mesh point index on the surface of the dielectric. This is normally equal to N_{A2} but can be increased to model the effect of a gap between the dielectric and the rings.

$$N_d := N_{A2}$$

Right hand boundary condition

$$P_{\text{sym}} := 2$$

Voltages on left-hand and right-hand strips

$$V_1 := 100$$

$$V_2 := 100$$

Maximum number of iterations

$$N_{\text{iter}} := 5000$$

The zero, $\pi/2$ and π modes can be modelled as follows

Zero mode:	$V_1 = 100$	$V_2 = 100$	$P_{\text{sym}} = 2$
$\pi/2$ mode	$V_1 = 100$	$V_2 = 0$	$P_{\text{sym}} = 0$
π mode	$V_1 = 100$	$V_2 = -100$	$P_{\text{sym}} = 2$

Calculation of voltages at the mesh points using a finite difference solution of Laplace's equation

The region below can be collapsed to allow the input data and the results to be on the screen simultaneously.



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VM := for i ∈ 0..Np
      for j ∈ 0..Ns
        Vi,j ← 0
      for n ∈ 1..Niter
        V0,0 ←  $\frac{4 \cdot V_{0,1} + 2 \cdot V_{1,0}}{6}$ 
        VNp,0 ←  $\frac{4 \cdot V_{Np,1} + P_{\text{sym}} \cdot V_{Np-1,0}}{6}$ 
        for i ∈ 1..Np - 1
          Vi,0 ←  $\frac{V_{i-1,0} + 4 \cdot V_{i,1} + V_{i+1,0}}{6}$ 
        for j ∈ 1..(Na1 - 1)
          V0,j ←  $\left[ 2 V_{1,j} + \left( 1 + \frac{1}{2 \cdot j} \right) V_{0,j+1} + \left( 1 - \frac{1}{2 \cdot j} \right) V_{0,j-1} \right] \cdot 0.25$ 
          VNp,j ←  $\left[ P_{\text{sym}} V_{Np-1,j} + \left( 1 + \frac{1}{2 \cdot j} \right) V_{Np,j+1} + \left( 1 - \frac{1}{2 \cdot j} \right) V_{Np,j-1} \right] \cdot 0.25$ 
          for i ∈ 1..Np - 1
            Vi,j ←  $\left[ V_{i+1,j} + \left( 1 + \frac{1}{2 \cdot j} \right) V_{i,j+1} + V_{i-1,j} + \left( 1 - \frac{1}{2 \cdot j} \right) V_{i,j-1} \right] \cdot 0.25$ 
        for j ∈ Na1..Na2
          for i ∈ 0..Np
            Vi,j ← V1 if i ≤ Nw2
            Vi,j ← V2 if i ≥ Np - Nw2
            for i ∈ (Nw2 + 1)..(Np - Nw2 - 1)
              Vi,j ←  $\left[ V_{i+1,j} + \left( 1 + \frac{1}{2 \cdot j} \right) V_{i,j+1} + V_{i-1,j} + \left( 1 - \frac{1}{2 \cdot j} \right) V_{i,j-1} \right] \cdot 0.25$  if j ≠ Nd

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Array indices are i for z and j for r.
Initially set all the mesh voltages to zero

Voltages on the axis.

Voltages at mesh points inside the rings

Voltages at mesh points in the
thickness of the rings

$V_{i,j} \leftarrow \frac{\left(1 + \frac{1}{2 \cdot j}\right) \epsilon_r \cdot V_{i,j+1} + \left(1 - \frac{1}{2 \cdot j}\right) V_{i,j-1} + \frac{(1 + \epsilon_r)}{2} \cdot (V_{i+1,j} + V_{i-1,j})}{2 \cdot (\epsilon_r + 1) + \frac{1}{2 \cdot j} \cdot (\epsilon_r - 1)} \quad \text{otherwise}$	
for $j \in \text{Na2} + 1 .. \text{Ns} - 1$	
$V_{0,j} \leftarrow \begin{cases} \left[2 V_{1,j} + \left(1 + \frac{1}{2 \cdot j}\right) V_{0,j+1} + \left(1 - \frac{1}{2 \cdot j}\right) V_{0,j-1} \right] \cdot 0.25 & \text{if } j \neq \text{Nd} \\ \frac{(1 + \epsilon_r) \cdot V_{1,j} + \left(1 + \frac{1}{2 \cdot j}\right) \epsilon_r \cdot V_{0,j+1} + \left(1 - \frac{1}{2 \cdot j}\right) V_{0,j-1}}{2 \cdot (\epsilon_r + 1) + \frac{1}{2 \cdot j} \cdot (\epsilon_r - 1)} & \text{otherwise} \end{cases}$	
$V_{\text{Np},j} \leftarrow \begin{cases} \left[\text{Psym } V_{\text{Np}-1,j} + \left(1 + \frac{1}{2 \cdot j}\right) V_{\text{Np},j+1} + \left(1 - \frac{1}{2 \cdot j}\right) V_{\text{Np},j-1} \right] \cdot 0.25 & \text{if } j \neq \text{Nd} \\ \frac{\frac{(1 + \epsilon_r) \cdot \text{Psym}}{2} \cdot V_{\text{Np}-1,j} + \left(1 + \frac{1}{2 \cdot j}\right) \epsilon_r \cdot V_{\text{Np},j+1} + \left(1 - \frac{1}{2 \cdot j}\right) V_{\text{Np},j-1}}{2 \cdot (\epsilon_r + 1) + \frac{1}{2 \cdot j} \cdot (\epsilon_r - 1)} & \text{otherwise} \end{cases}$	
for $i \in 1 .. \text{Np} - 1$	
$V_{i,j} \leftarrow \begin{cases} \left[V_{i+1,j} + \left(1 + \frac{1}{2 \cdot j}\right) V_{i,j+1} + V_{i-1,j} + \left(1 - \frac{1}{2 \cdot j}\right) V_{i,j-1} \right] \cdot 0.25 & \text{if } j \neq \text{Nd} \\ \frac{\left(1 + \frac{1}{2 \cdot j}\right) \epsilon_r \cdot V_{i,j+1} + \left(1 - \frac{1}{2 \cdot j}\right) V_{i,j-1} + \frac{(1 + \epsilon_r)}{2} \cdot (V_{i+1,j} + V_{i-1,j})}{2 \cdot (\epsilon_r + 1) + \frac{1}{2 \cdot j} \cdot (\epsilon_r - 1)} & \text{otherwise} \end{cases}$	
for $i \in 0 .. \text{Np}$	
$V_{i,\text{Ns}} \leftarrow 0$	
$\text{VM} \leftarrow V$	Voltages at mesh points between the rings and the shield
return VM	

Working equations

On the axis
$$V_{i,0} = \frac{1}{6} (V_{i+1,0} + 4V_{i,j+1} + V_{i-1,0})$$

In regions of uniform permittivity
$$V_{i,j} = \frac{1}{4} \left[V_{i+1,j} + \left(1 + \frac{1}{2j}\right) V_{i,j+1} + V_{i-1,j} + \left(1 - \frac{1}{2j}\right) V_{i,j-1} \right]$$

On the surface of the dielectric
$$V_{i,j} = \frac{\left(1 + \frac{1}{2j}\right) \epsilon_r V_{i,j+1} + \left(1 - \frac{1}{2j}\right) V_{i,j-1} + \left(\frac{1 + \epsilon_r}{2}\right) (V_{i+1,j} + V_{i-1,j})}{2(\epsilon_r + 1) + \frac{1}{2j}(\epsilon_r - 1)}$$

Calculation of the charge per unit length on the surfaces of the solution region

$$Q1 := \left[\sum_{i=0}^{Np2} \left(2 \cdot VM_{i, Ns-1} \right) - VM_{0, Ns-1} - VM_{Np2, Ns-1} \right] \cdot \pi \cdot \epsilon_r \cdot \left(Ns - \frac{1}{2} \right)$$

$$Q1 = 1.3 \times 10^5$$

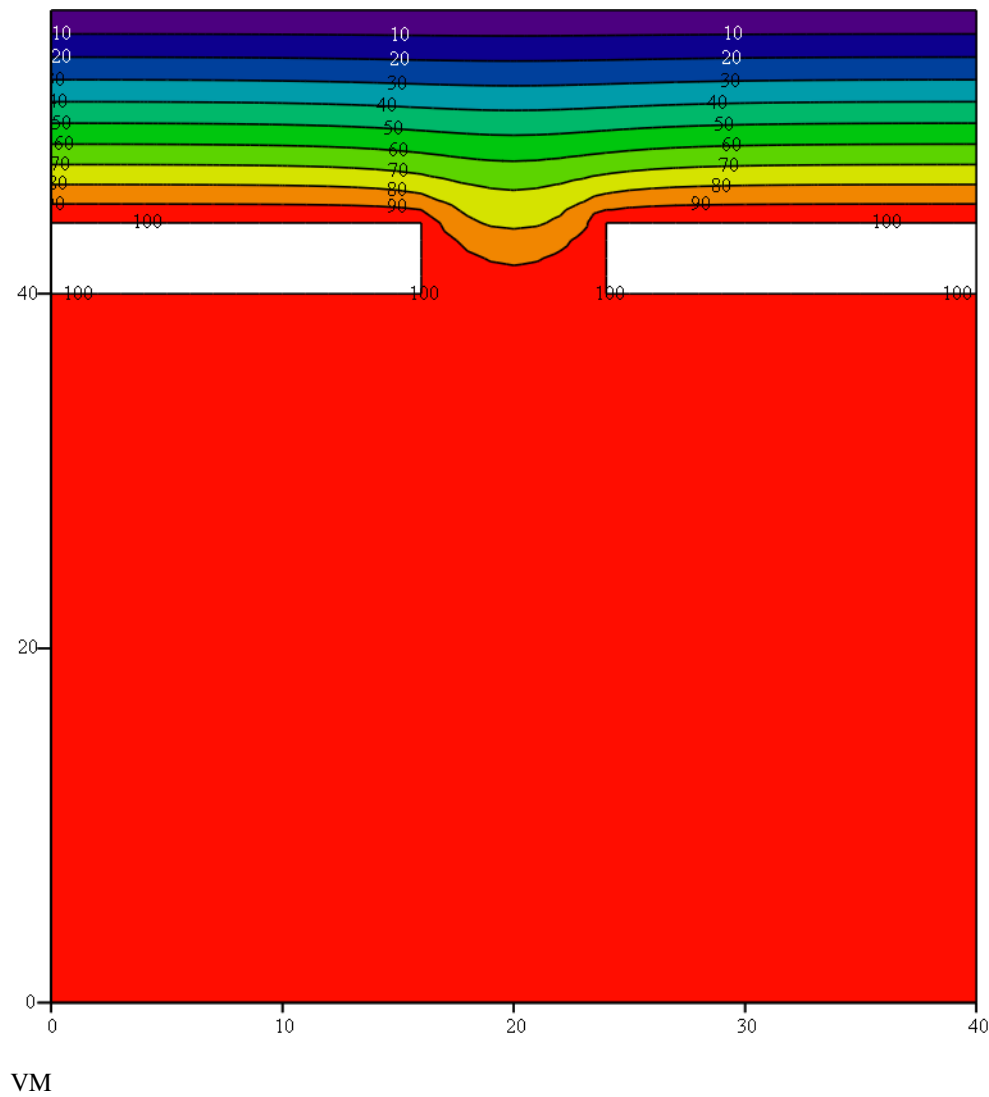
$$Q2 := \frac{\pi}{4} \cdot \sum_{j=0}^{Nd-1} \left[\left(VM_{Np2-1, j} - VM_{Np2+1, j} + VM_{Np2-1, j+1} - VM_{Np2+1, j+1} \right) \cdot (2 \cdot j + 1) \right]$$

$$Q2 = -0$$

$$Q3 := \frac{\pi \cdot \epsilon_r}{4} \cdot \sum_{j=Nd}^{Ns-1} \left[\left(VM_{Np2-1, j} - VM_{Np2+1, j} + VM_{Np2-1, j+1} - VM_{Np2+1, j+1} \right) \cdot (2 \cdot j + 1) \right]$$

$$Q3 = -0$$





NB Care should be taken that the routine has converged completely.

Capacitance per unit length of the structure divided by ϵ_0

$$\text{Capacitance} := \frac{Q1 + Q2 + Q3}{V_1 \cdot Np2}$$

Capacitance = 63.09

Capacitance per unit length divided by ϵ_0 of a coaxial line with inner and outer radii $(a_1 + t/2)$ and s .

$$C_{00} := \frac{2 \cdot \pi \cdot \epsilon_r}{\ln\left(\frac{s}{a_1 + 0.5 \cdot t}\right)}$$

$C_{00} = 54.60$

$$\alpha_C := \frac{\text{Capacitance}}{C_{00}}$$

$\alpha_C = 1.155$

The results of calculations with $p = 10\text{mm}$, $a = 10\text{mm}$, $t = 1\text{mm}$ and $\epsilon_r = 1$ were computed and stored in the matrices below for a range of values of w/p and s/p .

$$\begin{aligned}
 & \begin{pmatrix} 0.1 \\ 0.2 \\ 0.3 \\ 0.4 \\ 0.5 \\ 0.6 \\ 0.7 \\ 0.8 \\ 0.9 \\ 1.0 \end{pmatrix} \quad \alpha_{14} := \begin{pmatrix} 0.679 \\ 0.785 \\ 0.877 \\ 0.957 \\ 1.027 \\ 1.086 \\ 1.133 \\ 1.167 \\ 1.188 \\ 1.188 \end{pmatrix} \cdot \frac{\ln\left(\frac{14}{11}\right)}{\ln\left(\frac{14}{10.5}\right)} \quad \alpha_{20} := \begin{pmatrix} 0.823 \\ 0.889 \\ 0.939 \\ 0.979 \\ 1.011 \\ 1.036 \\ 1.055 \\ 1.068 \\ 1.076 \\ 1.076 \end{pmatrix} \cdot \frac{\ln\left(\frac{20}{11}\right)}{\ln\left(\frac{20}{10.5}\right)} \quad \alpha_{28} := \begin{pmatrix} 0.876 \\ 0.924 \\ 0.959 \\ 0.986 \\ 1.007 \\ 1.024 \\ 1.036 \\ 1.044 \\ 1.049 \\ 1.049 \end{pmatrix} \cdot \frac{\ln\left(\frac{28}{11}\right)}{\ln\left(\frac{28}{10.5}\right)}
 \end{aligned}$$

The multiplying factors convert the values of α from those computed at the mean radius of the helix to those at the outer radius.

Figure 4.19

