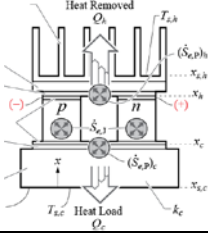
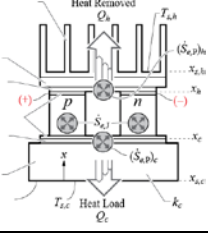


Errata for Essentials of Heat Transfer

Page	Location	Correction	
		Original	Revised
24	under figure	Figure 1.4(a) Figure 1.4	Figure 1.5(a) Figure 1.5
25	(1.12) and (1.13)	$q = \rho c_p u$	$q = \rho c_p u T$
57	Problem 1.13(a)	For the conditions given below, determine ...	For the conditions given below, plot
57	Problem 1.13(a)	$\tau = \rho c_p V R_t$	$\tau = \rho c_v V R_t$
72	Paragraph 2, lines 6-7	..medium 1 (for example a gas), but radiation or convection in other medium (for example a solid).	..medium 1 (for example a solid), but radiation or convection in other medium (for example a gas).
72	Last line	This relationhas allowed us...	This relation has allowed us...
90	Example 2.6	$\dot{s}_{r,c} = -2.942 \times 10^{16} \rho_F^{-0.3} \rho_O^{1.3} \dots$	$\dot{s}_{r,c} = -2.942 \times 10^{16} \rho_F^{-0.3} \rho_O^{1.3} \dots$
91	Line 10	The constants are given in Example 2.5 and ...	The constants are given in Example 2.6 and ...
92	Section 2.3.1(C)	In Section (C), Nuclear Fission Reaction with an example (Examples 2.8).	In Section (C), Nuclear Fusion Reactionwith an example (Examples 2.8).
126	Problem 2.4	... $c_{p,s} = 1,930 \text{ J/kg-K}$, ...	... $c_{p,s} = 1,930 \text{ J/kg-K}$, ...
128	Problem 2.6.(a)	$h_p f = h_p \frac{\lambda}{c}$	$h_p f = h_p \frac{c}{\lambda}$
168	Example 3.2	8,315(J/kg-K)/28.964(kg/kmole)	8,315(J/kmole-K)/28.964(kg/kmole)
231	In Figure 3.28(b)		
233	3 lines from bottom	... $T = 300$ from Table C.14).	... $T = 300 \text{ K}$ from Table C.14).
234	2 lines from bottom	... $\alpha_s J_e (T_h - T_c)$. The optimum ...	... $\alpha_s J_e (T_h - T_c)$. (new paragraph) The optimum ..
236	Example 3.13	Use $T_h = 308.60 \text{ K}$.	Use $T_h = 308.6 \text{ K}$.
249	Example 3.16(a)	$\frac{T(r=0, \text{Fo}_R = 0.5371) - \tau(t=0)}{T_s - T(t=0)}$	$\frac{T(r=0, \text{Fo}_R = 0.5371) - T(t=0)}{T_s - T(t=0)}$
254	Paragraph 3. [right after (3.144)]	... where from (3.136) $\partial \eta / \partial x = 1/(2at)^{1/2}$ and ...	... where from (3.136) $\partial \eta / \partial x = 1/(4at)^{1/2}$ and ...
254	Paragraph 4, 3 lines from bottom	$q_{\rho c_p k}$ tends to zero. ...	$q_{\rho c k}$ tends to zero. ...
255	Table 3.6	$Q_{pck}(t) = A_k q_{pck}$, $W = [T(t=0) - T_s]/R_{pck}(t)$	$Q_{pck}(t) = A_k q_{pck} = [T(t=0) - T_s]/R_{pck}(t)$ (W)
290	Problem 3.25, paragraph 2	Figure Pr.3.25 shows a thin circular heater used to ...	Figure Pr.3.25 shows a thin heater used to ...
310	Problem 3.50	..., for molds (i), (ii) and (iii) .	..., for molds (a), (b) and (c) .
326	Section 4.1.2, 3 lines from bottom	... $n_{ph} h_p f = n_{ph} h_p \lambda / c$, where ...	... $n_{ph} h_p f = n_{ph} h_p c / \lambda$, where ...
330	(4.6)	$\dots = \frac{2\pi^5 k_B^4}{15 h_p^3 c_o^2} \equiv \sigma_{SB} T^4 (\text{W/m}^2)$	$\dots = \frac{2\pi^5 k_B^4}{15 h_p^3 c_o^2} T^4 \equiv \sigma_{SB} T^4 (\text{W/m}^2)$
340	Line 3	Commonly, nlambda and klambda are	Commonly, n_λ and κ_λ are also called...

		also called...	
353	Figure 4.11(d)	$F_{2-2} = 1 - \frac{1}{R^*} + \dots$	$F_{2-2} = 1 - \frac{1}{R^*} + \dots$
356	Table 4.3	$Q_{r,i} = A_{r,i} q_{r,i}$ $\mathbf{W} = [E_{b,i} - (q_{r,o})_i] / (R_{r,\varepsilon})_i$ $Q_{r,i-j} = A_{r,i} q_{r,i-j}$, $\mathbf{W}$ $\mathbf{W} = [(q_{r,o})_i - (q_{r,o})_j] / (R_{r,F})_{i-j}$	$Q_{r,i} = A_{r,i} q_{r,i}$, $\mathbf{W}$ $= [E_{b,i} - (q_{r,o})_i] / (R_{r,\varepsilon})_i$ $Q_{r,i-j} = A_{r,i} q_{r,i-j}$, $\mathbf{W}$ $= [(q_{r,o})_i - (q_{r,o})_j] / (R_{r,F})_{i-j}$
373	second equation	1.273	127.3
381	Example 4.13(a)	$Q_{k,H-1} = \dots$	$Q_{k,H-1} = \dots$
412	Problem 4.44(a)	$q_{r,x} = \frac{4\varepsilon_r \sigma_{SB} T^3 (T'_f - T_2)}{2 - \varepsilon_r}$	$q_{r,x} = \frac{4\varepsilon_r \sigma_{SB} T^3 (T'_f - T_2)}{2 - \varepsilon_r}$
438	Between (6.23) and (6.24)	... through $\partial T_f / \partial y _{y=0+}$.	... through $\partial T_f / \partial y _{y=0+}$.
438	(6.24)	$\frac{\partial T_f}{\partial y} \Big _{y=0^+} = - \frac{\text{Pe}_L^{1/2}}{\pi} \frac{T_s - T_{f,\infty}}{L}$	$\frac{\partial T_f}{\partial y} \Big _{y=0^+} = - \frac{\text{Pe}_L^{1/2}}{\pi^{1/2}} \frac{T_s - T_{f,\infty}}{L^{1/2}}$
439	Between (6.26) and (6.27)	... as the product $(k_f \rho c_p)_f u_{f,\infty}$ increases.	... as the product $(k \rho c_p)_f u_{f,\infty}$ increases.
441	Figure 6.6		x axis: remove every other tick mark, the labels should be $10^2, 10^3, 10^4, 10^5$
466	First paragraph in Section 6.5	This is due to the interaction of the gravity vector $\mathbf{g}$ and the ...	This is due to the interaction of the gravity vector $\mathbf{g}$ and the ...
471	(6.80)	... = $\rho_f g \beta_f (T_f - T_{f,\infty})$	... = $\rho_f g \beta_f (T_f - T_{f,\infty})$
473	Between (6.85) and (6.86)	Since we assume that $\text{Gr}_L \geq 0$, whenever $T_{f,\infty} < T_s$, ...	Since we assume that $\text{Gr}_L \geq 0$, whenever $T_{f,\infty} > T_s$, ...
473	(6.86)	$u_f^*(x^* = 0, y^*) = v_f^*(x^* = 0, y^*)$, ...	$u_f^*(x^* = 0, y^*) = v_f^*(x^* = 0, y^*) = 0$, ...
474	Between (6.87) and (6.88)	Compared to (6.47), $k_f \partial T_f / \partial y _{y=0+} = \dots$	Compared to (6.47), $\partial T_f / \partial y _{y=0+} = \dots$
485	(6.99)	$\langle \text{Nu} \rangle_L = \frac{L}{A_{ku} \langle R_{ku} \rangle_L k_l} = \frac{\text{Ja}_L^2 \text{Bo}_L^{1/2}}{a_s^3 \text{Pr}_l^n}$	$\langle \text{Nu} \rangle_L = \frac{L}{A_{ku} \langle R_{ku} \rangle_L k_l} = \frac{\text{Ja}_L^2 \text{Bo}_L^{1/2}}{a_s^3 \text{Pr}_l^{n-1}}$
512	Example 6.13(b)	where from Table 3.1 $R_{k,1-2} = \frac{\ln(R_2 / R_1)}{2\pi L k_s}$ Table 3.1	where from Table 3.2 $R_{k,1-2} = \frac{\ln(R_2 / R_1)}{2\pi L k_s}$ Table 3.2
529	Example 6.16	Figure Ex. 6.16	$Q_{r,1-\infty}$ and $Q_{ku,1-\infty}$ are not zero
534	Problem 6.1(f)	...(ideal insulation)? $\text{vspace*}{-6pt}$	...(ideal insulation)? $\text{vspace*}{-6pt}$
601	Table 7.5. (below "Iso-diametral Cylinders")	Add: For All Geometries $\left\{ \begin{array}{l} \langle \text{Nu} \rangle_{D,p} = \frac{D_p / k_f}{A_{ku} \langle R_{ku} \rangle_{D,p}} \left(\frac{\varepsilon}{1 - \varepsilon} \right) = 2 + (0.4 \text{Re}_{D,p}^{1/2} + 0.2 \text{Re}_{D,p}^{2/3}) \text{Pr}^{0.4} \\ D_p = \frac{6V_s}{A_{ku}} = \frac{6V(1 - \varepsilon)}{A_{ku}}, \text{Re}_{D,p} = \frac{\rho_f \langle u_f \rangle D_p}{\mu_f (1 - \varepsilon)}, \text{NTU} = \frac{1}{\langle R_{ku} \rangle_{D,p} (\dot{M} c_p)_f} \end{array} \right.$	
610	Example 7.4	Start from (2.72)...	Start from (2.9)...
610	Example 7.4	Starting from (2.72)...	Starting from (2.9)...
612	Example 7.5	NTU	-NTU
616	(7.56)	... $q_{<ku,h>} + dq_{u,h} / dx$	... $q_{ku,h} + d<q_{u,h}> / dx$
617	(7.64)	=	= -
669	Problem 4.7(c)	... = $3.680 \times 10^{-4} \text{ W/m}^2 \cdot \mu\text{m}$	... = $3.368 \times 10^{-4} \text{ W/m}^2 \cdot \mu\text{m}$
673	Problem 6.53(c) and (d)	= -2.036 W, and = -0.0006069 K/s	= -20.96 W, and = -0.03306 K/s
Online	Table C.27, under $k_l \quad k_g$	mW/m-K	W/m-K