

3.2 Noise

Outline

- Thermal noise, noise power and noise temperature
- Noise in RLC single-ports
- Noise in diodes and photodiodes
- 2-port and multi-port noise parameters
- Noise temperature and noise parameter measurements

Thermal noise, noise power, noise temp

- 2 definitions of T_n

- $T_n \equiv T$ of resistor for given p_n

- $T_n \equiv \frac{p_n}{k}$

- 3 definitions of noise power density, p_n

- Planck,

$$p_n^{Planck} = kT \left[\frac{\frac{hf}{kT}}{e^{\frac{hf}{kT}} - 1} \right]$$

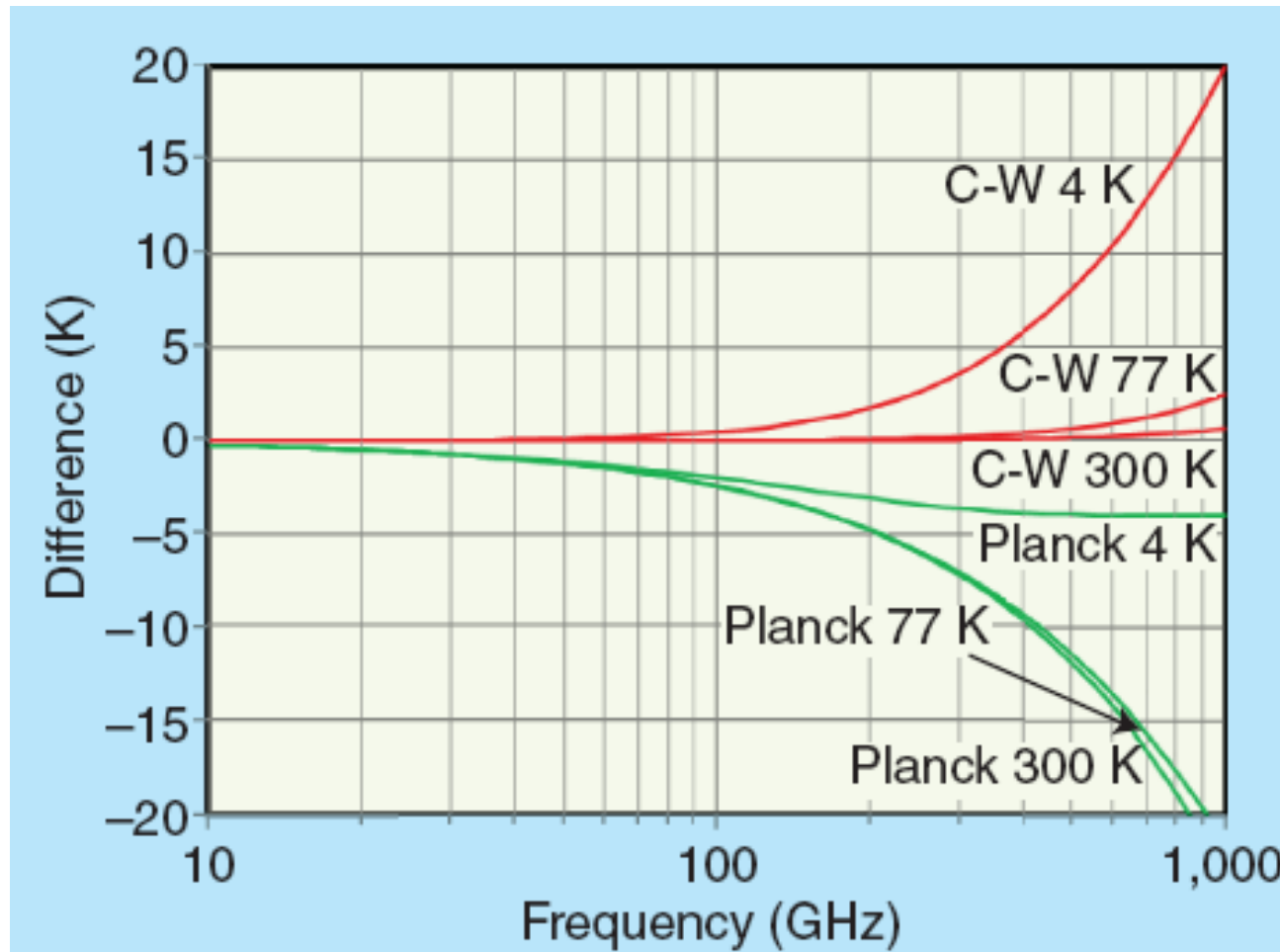
- Rayleigh-Jeans (from Planck),

$$p_n^{R-J} = kT$$

- Callen-Welton

$$p_n^{C-W} = p_n^{Planck} + p_n^{vac} = kT \left[\frac{\frac{hf}{kT}}{e^{\frac{hf}{kT}} - 1} \right] + \frac{hf}{2}$$

Difference between T_n and T for a resistor



$$T_n^{R-J} = T$$

$$T_n^{Planck} = T \left[\frac{\frac{hf}{kT}}{e^{\frac{hf}{kT}} - 1} \right]$$

$$T_n^{C-W} = T \left[\frac{\frac{hf}{kT}}{e^{\frac{hf}{kT}} - 1} \right] + \frac{hf}{2k}$$

A.R. Kerr and J. Randa, "Thermal Noise and Noise Measurements – A 2010 Update," IEEE Microwave Magazine, pp.40-52, October 2010.

Lossy Single-Port Noise: Resistor

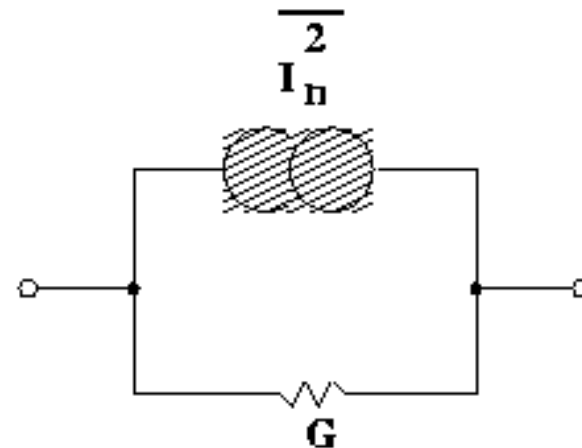
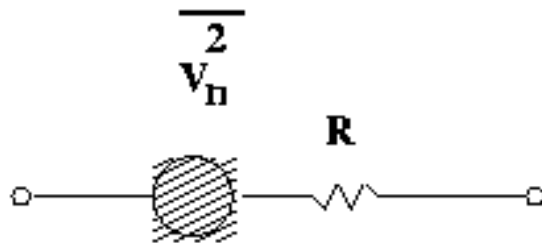
$$\overline{v_n^2} = 4kT\Delta f R$$

$$R = \frac{1}{G}$$

$$k = 1.38 \times 10^{-23} \text{ J K}^{-1}$$

$$\overline{i_n^2} = 4kT\Delta f G$$

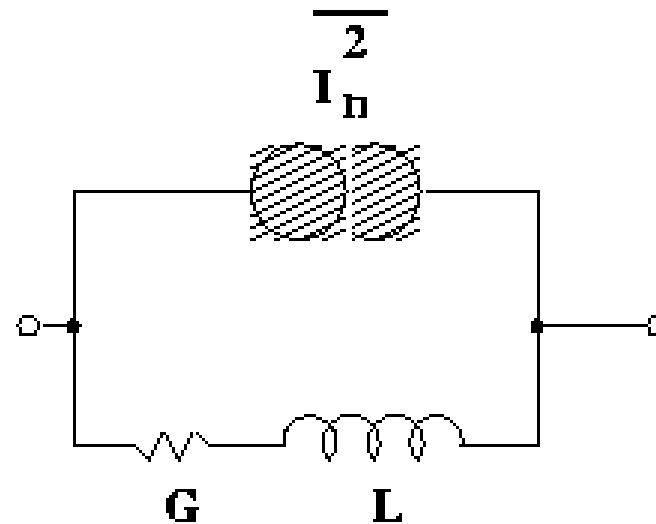
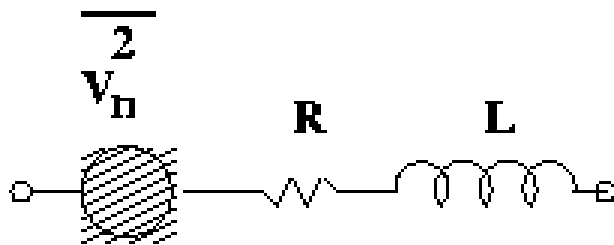
$$v_n(f) = \sqrt{\frac{R}{1 \text{ k}\Omega}} \times 4.06 \frac{\text{nV}}{\sqrt{\text{Hz}}}$$



Lossy Single-Port Resistor + Inductor

$$\overline{v_n^2} = 4kT\Delta f R \quad R = \frac{1}{G}$$

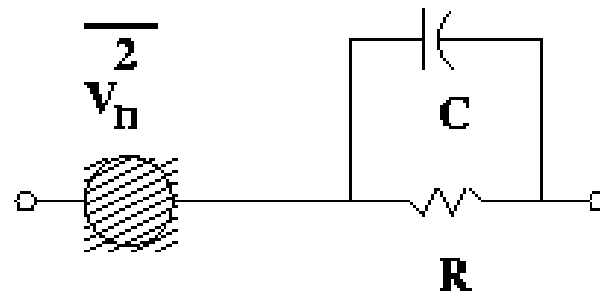
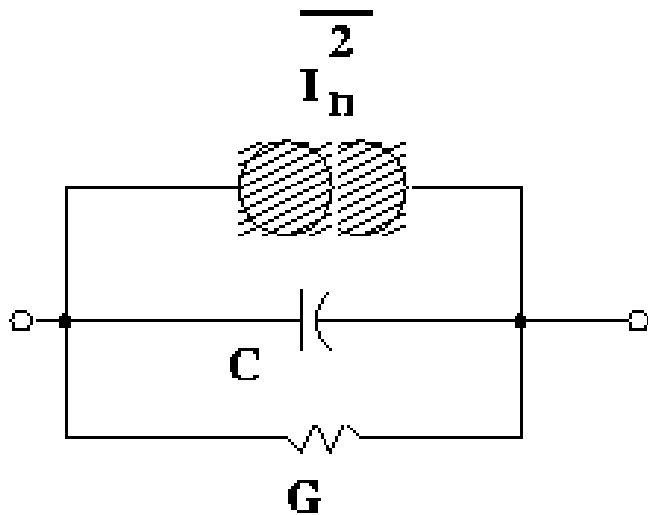
$$\overline{i_n^2} = \frac{\overline{v_n^2}}{R^2 + \omega^2 L^2} = \frac{4kT\Delta f G}{1 + \omega^2 L^2 G^2}$$



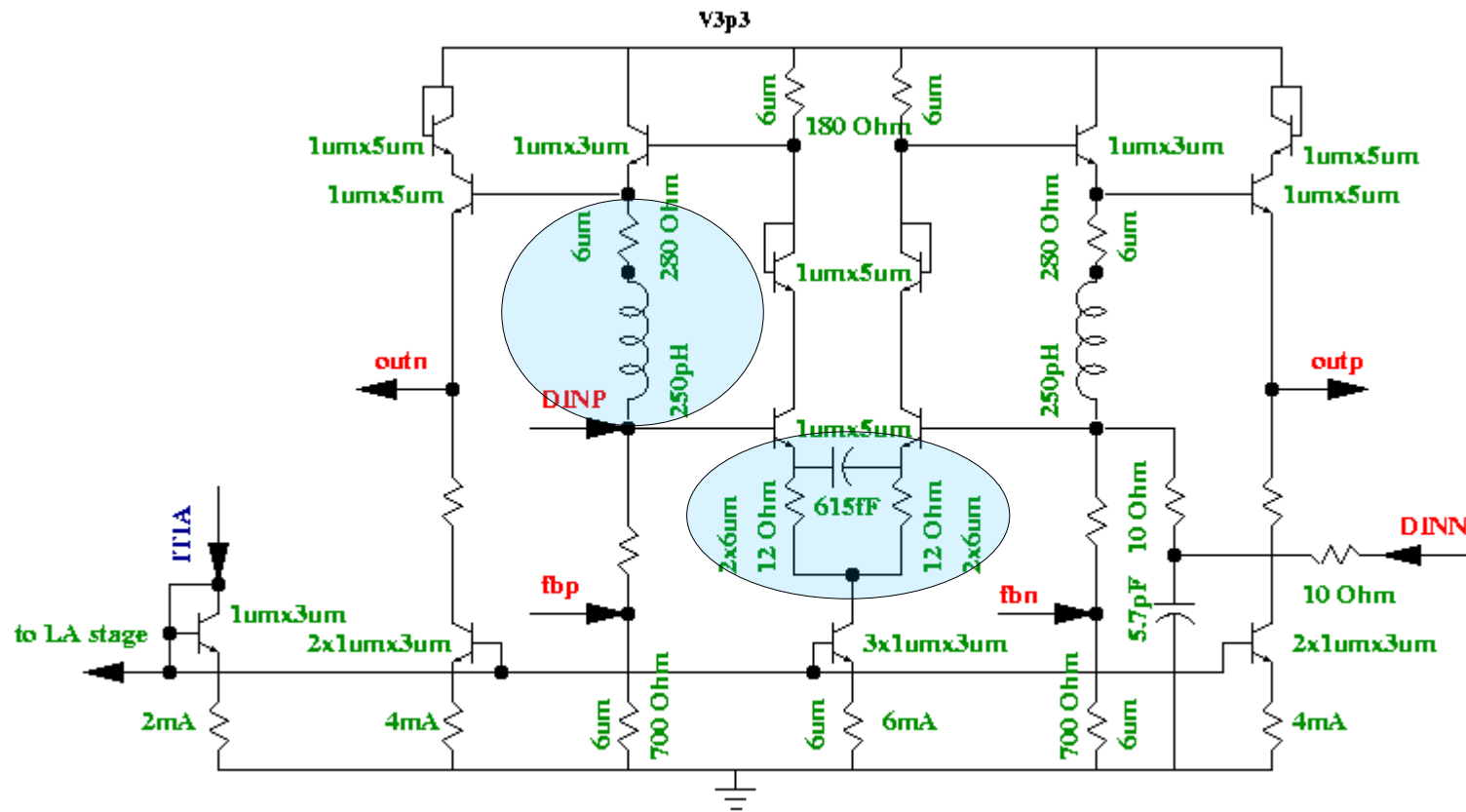
Lossy Single-Port Noise: Resistor || Capacitor

$$\overline{i_n^2} = 4kT\Delta f G \quad R = \frac{1}{G}$$

$$\overline{V_n^2} = \frac{\overline{i_n^2}}{G^2 + \omega^2 C^2} = \frac{4kT\Delta f R}{1 + \omega^2 C^2 R^2}$$



Example: series L-R series + shunt C-R

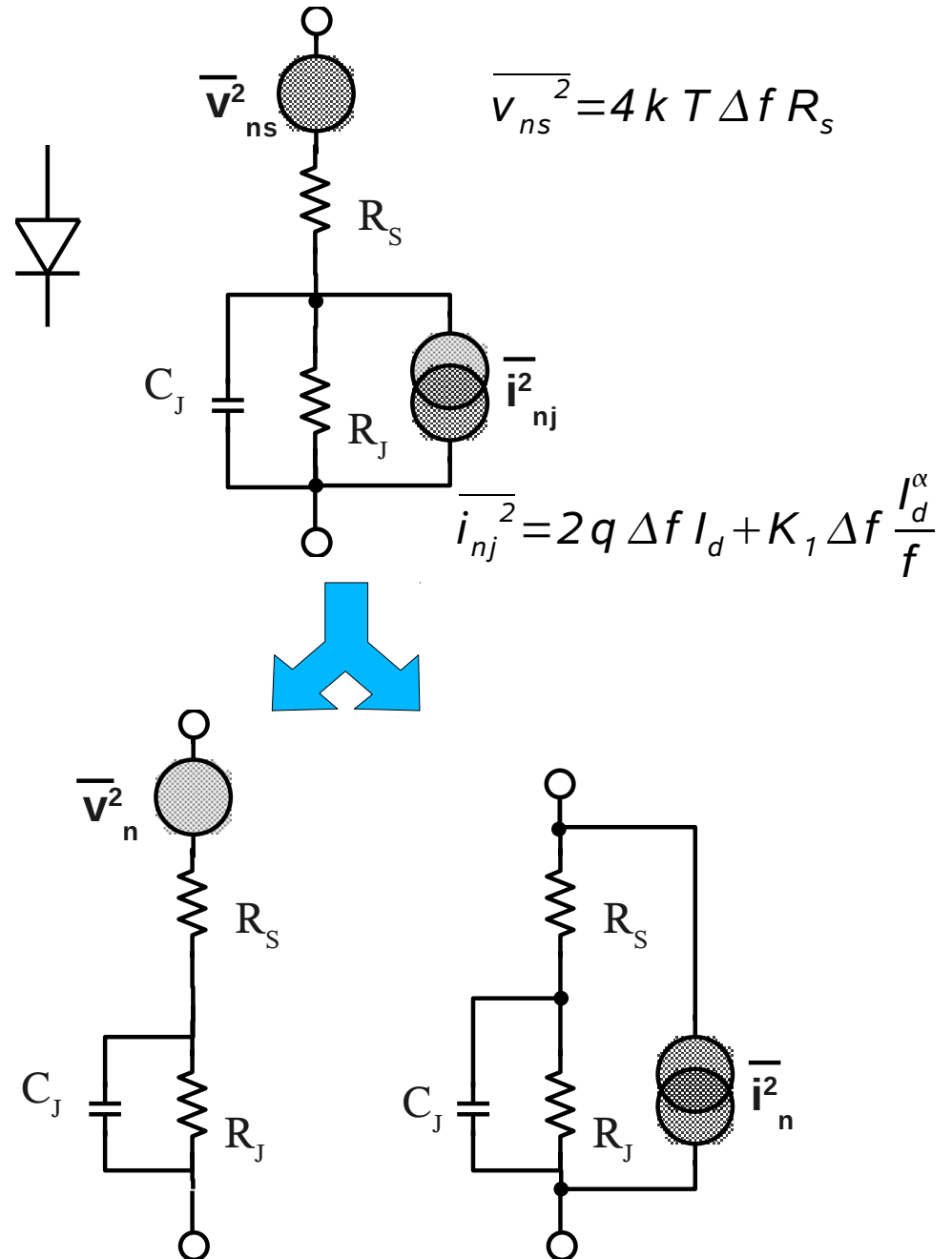


Total current = 18mA + 2mA shared with T1A and t-line transmitter

Diode Noise

- Intrinsic noise sources i_{nj} , v_{ns}
- Equivalent input thermal noise sources: v_n or i_n
- Equivalent noise conductance

$$G_e \stackrel{\text{def}}{=} \frac{\overline{i_n^2}}{4kT\Delta f} \approx \frac{qI_d}{2kT} = \frac{1}{2R_j}$$



Photodetectors

- PIN diodes: $M = 1$, $F(M) = 1$
- APDs: $M = 10..50$, $F(M) = 5 .. 10$

where: M is the multiplication factor and

$F(M)$ is the noise factor of the photo-diode

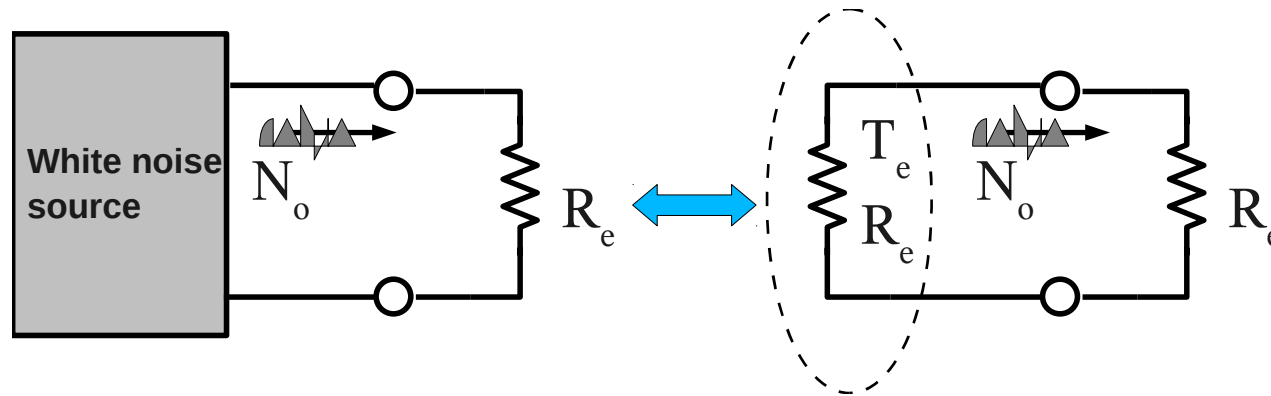
$I_{ph} = RMP$; R = diode responsivity and P = optical power

$$\overline{i_{n,ph}^2} = 2qI\Delta f = 2q\Delta f (RMP + MI_{dark})MF(M)$$

$$G_{seq} = \frac{(RP + I_{dark})M^2 F(M)}{\frac{2kT}{q}}$$

$$P_{min} = \frac{1}{R} \times \sqrt{2q\Delta f I_{dark} F(M)}$$

Noise source T_e and ENR



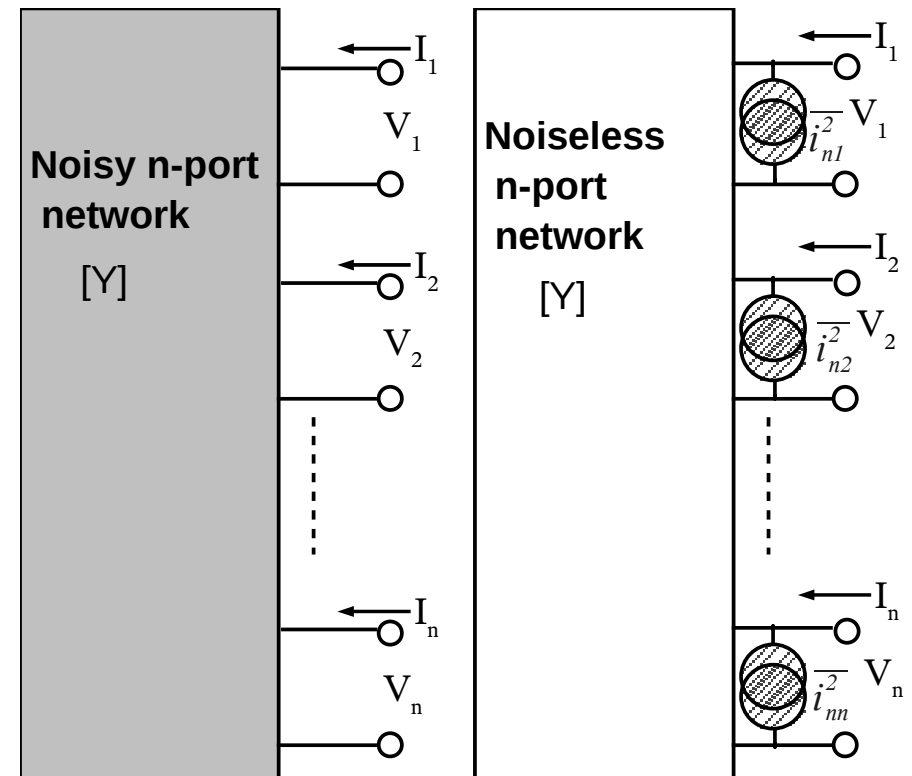
- T_e = equivalent (thermal) noise temperature of a white noise source
- ENR = excess noise ratio $ENR(dB) = 10 \log_{10} \left(\frac{T_e - T_0}{T_0} \right)$
- T_0 = reference temperature, typically 290 °K.

Multi-port noise representations: Y-params

- One noise current source exiting each port
- Y correlation matrix

$$\begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_n \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} & \cdot & \cdot & Y_{1n} \\ Y_{21} & Y_{22} & \cdot & \cdot & Y_{2n} \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ Y_{n1} & Y_{n2} & \cdot & \cdot & Y_{nn} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ \cdot \\ \cdot \\ V_n \end{bmatrix} + \begin{bmatrix} i_{n1} \\ i_{n2} \\ \cdot \\ \cdot \\ i_{nn} \end{bmatrix}$$

$$[C_y] = \begin{bmatrix} \langle i_{n1}, i_{n1}^* \rangle & \langle i_{n1}, i_{n2}^* \rangle & \cdot & \cdot & \langle i_{n1}, i_{nn}^* \rangle \\ \langle i_{n2}, i_{n1}^* \rangle & \langle i_{n2}, i_{n2}^* \rangle & \cdot & \cdot & \langle i_{n2}, i_{nn}^* \rangle \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \langle i_{nn}, i_{n1}^* \rangle & \langle i_{nn}, i_{n2}^* \rangle & \cdot & \cdot & \langle i_{nn}, i_{nn}^* \rangle \end{bmatrix}$$



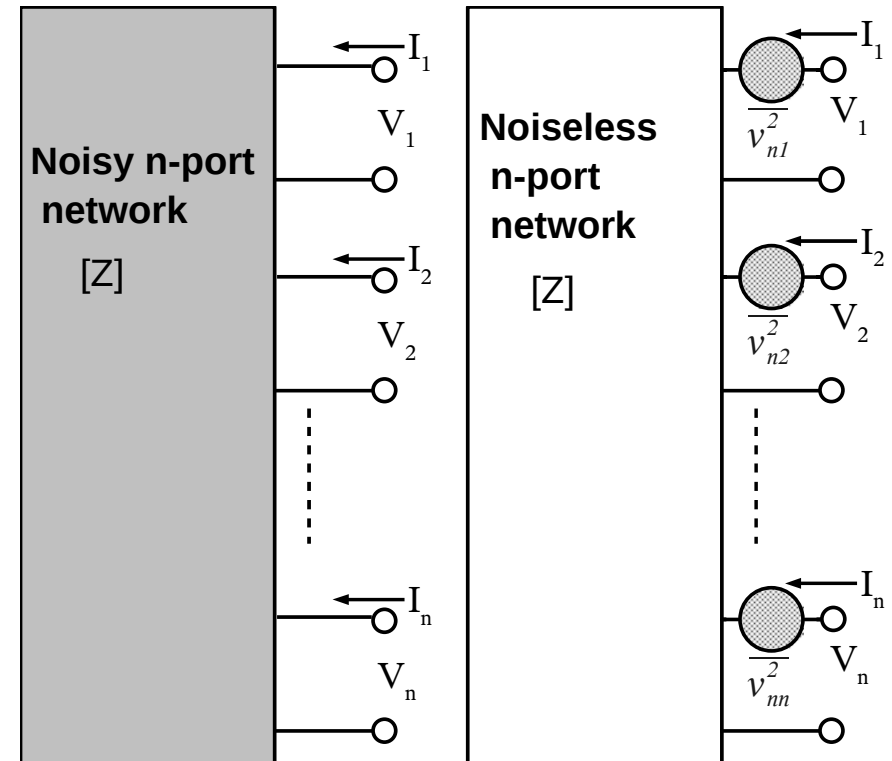
For passive network: $[C_y] = 4 kT \Delta f \text{Re}\{[Y]\}$

Multi-port noise representations: Z-params

- One noise voltage source at each port
- Z correlation matrix

$$\begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_n \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} & \cdot & \cdot & Z_{1n} \\ Z_{21} & Z_{22} & \cdot & \cdot & Z_{2n} \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ Z_{n1} & Z_{n2} & \cdot & \cdot & Z_{nn} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ \cdot \\ \cdot \\ I_n \end{bmatrix} + \begin{bmatrix} v_{n1} \\ v_{n2} \\ \cdot \\ \cdot \\ v_{nn} \end{bmatrix}$$

$$[C_Z] = \begin{bmatrix} \langle v_{n1}, v_{n1}^* \rangle & \langle v_{n1}, v_{n2}^* \rangle & \cdot & \cdot & \langle v_{n1}, v_{nn}^* \rangle \\ \langle v_{n2}, v_{n1}^* \rangle & \langle v_{n2}, v_{n2}^* \rangle & \cdot & \cdot & \langle v_{n2}, v_{nn}^* \rangle \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \langle v_{nn}, v_{n1}^* \rangle & \langle v_{nn}, v_{n2}^* \rangle & \cdot & \cdot & \langle v_{nn}, v_{nn}^* \rangle \end{bmatrix}$$



For passive network: $[C_Z] = 4 kT \Delta f \text{Re}\{[Z]\}$

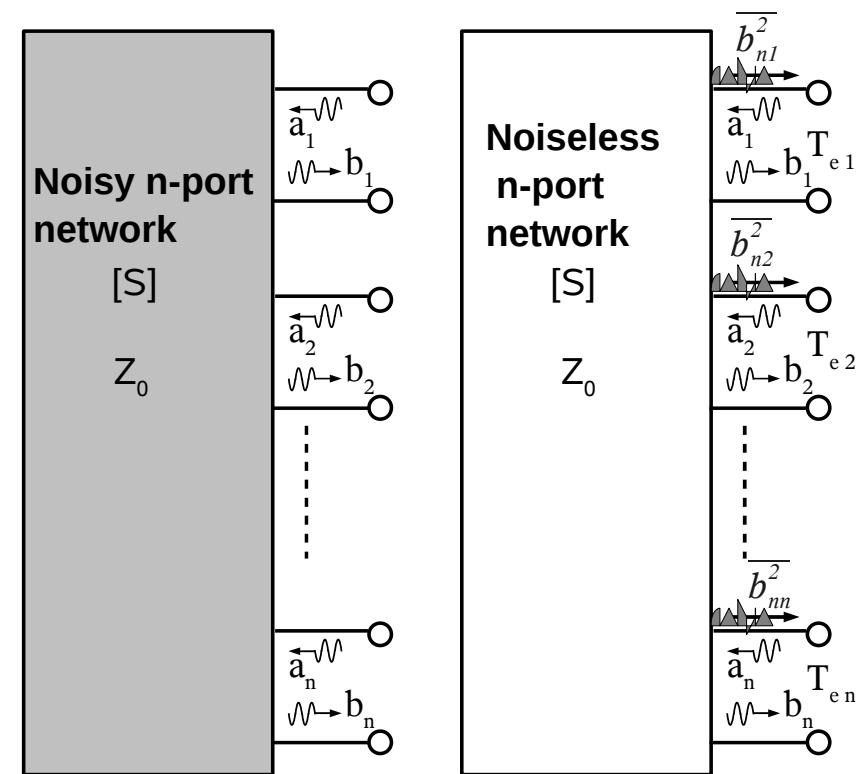
Multi-port noise representations: noise wave

- One noise wave emanating from each port
- wave correlation matrix

$$\begin{bmatrix} b_1 \\ b_2 \\ \vdots \\ b_n \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} & \cdot & \cdot & S_{1n} \\ S_{21} & S_{22} & \cdot & \cdot & S_{2n} \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ S_{n1} & S_{n2} & \cdot & \cdot & S_{nn} \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ \cdot \\ \cdot \\ a_n \end{bmatrix} + \begin{bmatrix} b_{n1} \\ b_{n2} \\ \cdot \\ \cdot \\ b_{nn} \end{bmatrix}$$

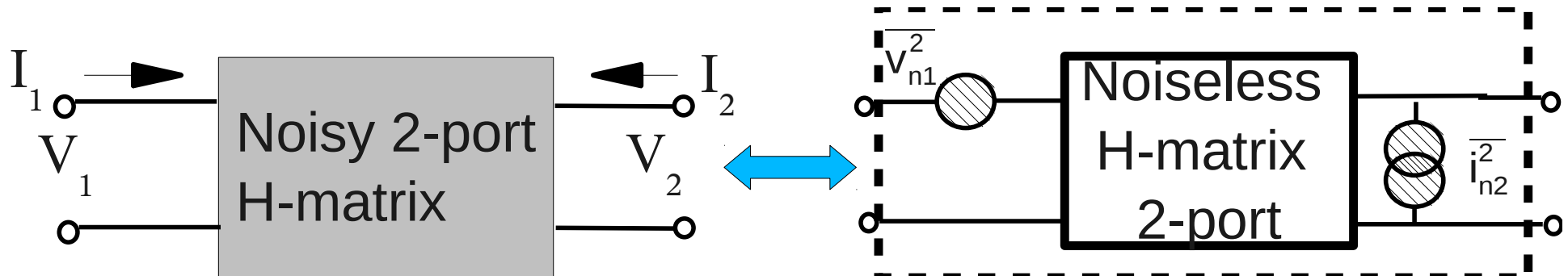
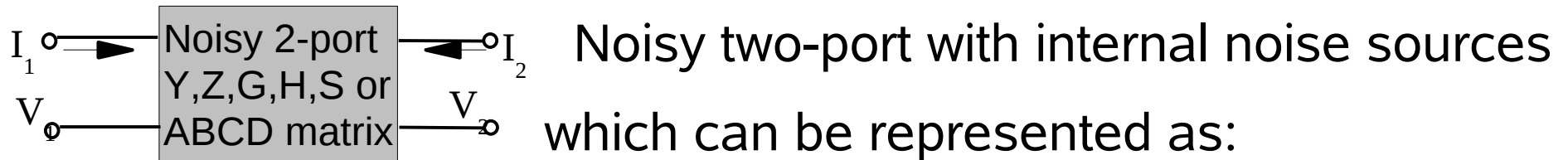
$$[C_S] = \begin{bmatrix} \langle b_{n1}, b_{n1}^* \rangle & \langle b_{n1}, b_{n2}^* \rangle & \cdot & \cdot & \langle b_{n1}, b_{nn}^* \rangle \\ \langle b_{n2}, b_{n1}^* \rangle & \langle b_{n2}, b_{n2}^* \rangle & \cdot & \cdot & \langle b_{n2}, b_{nn}^* \rangle \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \langle b_{nn}, b_{n1}^* \rangle & \langle b_{nn}, b_{n2}^* \rangle & \cdot & \cdot & \langle b_{nn}, b_{nn}^* \rangle \end{bmatrix}$$

For passive network:



$$[C_S] = k T \Delta f ([U] - [S][S]^+)$$

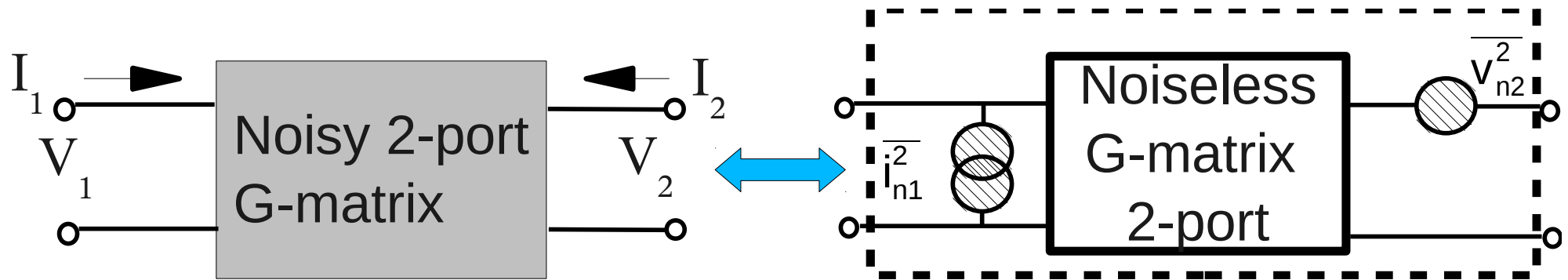
Other Noisy 2-Port (only) Correlation Matrices



$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} H_{11} & H_{12} \\ H_{21} & H_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix} + \begin{bmatrix} v_{n1} \\ i_{n2} \end{bmatrix}$$

$$[C_h] = \begin{bmatrix} \langle v_{n1}, v_{n1}^* \rangle & \langle v_{n1}, i_{n2}^* \rangle \\ \langle i_{n2}, v_{n1}^* \rangle & \langle i_{n2}, i_{n2}^* \rangle \end{bmatrix}$$

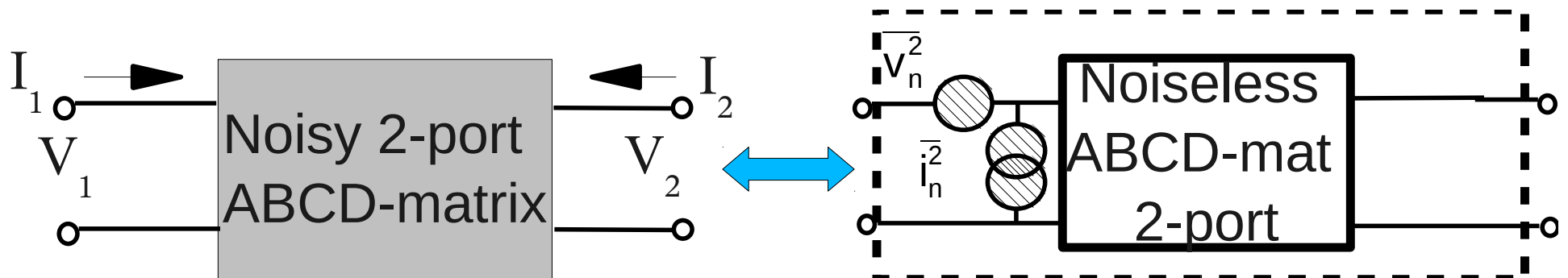
Two-port Correlation Matrices: G



$$\begin{bmatrix} I_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} G_{11} & G_{12} \\ G_{21} & G_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ I_2 \end{bmatrix} + \begin{bmatrix} i_{n1} \\ v_{n2} \end{bmatrix}$$

$$[C_g] = \begin{bmatrix} \langle i_{n1} & i_{n1}^* \rangle & \langle i_{n1} & v_{n2}^* \rangle \\ \langle v_{n2} & i_{n1}^* \rangle & \langle v_{n2} & v_{n2}^* \rangle \end{bmatrix}$$

Correlation Matrices: ABCD



$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix} + \begin{bmatrix} v_n \\ i_n \end{bmatrix}$$

$$[C_A] = \begin{bmatrix} \langle v_n & v_n^* \rangle & \langle v_n & i_n^* \rangle \\ \langle i_n & v_n^* \rangle & \langle i_n & i_n^* \rangle \end{bmatrix}$$

Noise Correlation Matrix Transformations

$$[C_z] = \begin{bmatrix} 1 & -Z_{11} \\ 0 & -Z_{22} \end{bmatrix} [C_A] \begin{bmatrix} 1 & 0 \\ -Z_{11}^* & -Z_{22}^* \end{bmatrix}; \quad [C_y] = \begin{bmatrix} -Y_{11} & 1 \\ -Y_{22} & 0 \end{bmatrix} [C_A] \begin{bmatrix} -Y_{11}^* & -Y_{22}^* \\ 1 & 0 \end{bmatrix}$$

$$[C_z] = [Z][C_y][Z]^+; \quad [C_z] = ([U] + [Z])[C_s]([U] + [Z])^+$$

$$[C_y] = [Y][C_z][Y]^+; \quad [C_y] = ([U] + [Y])[C_s]([U] + [Y])^+$$

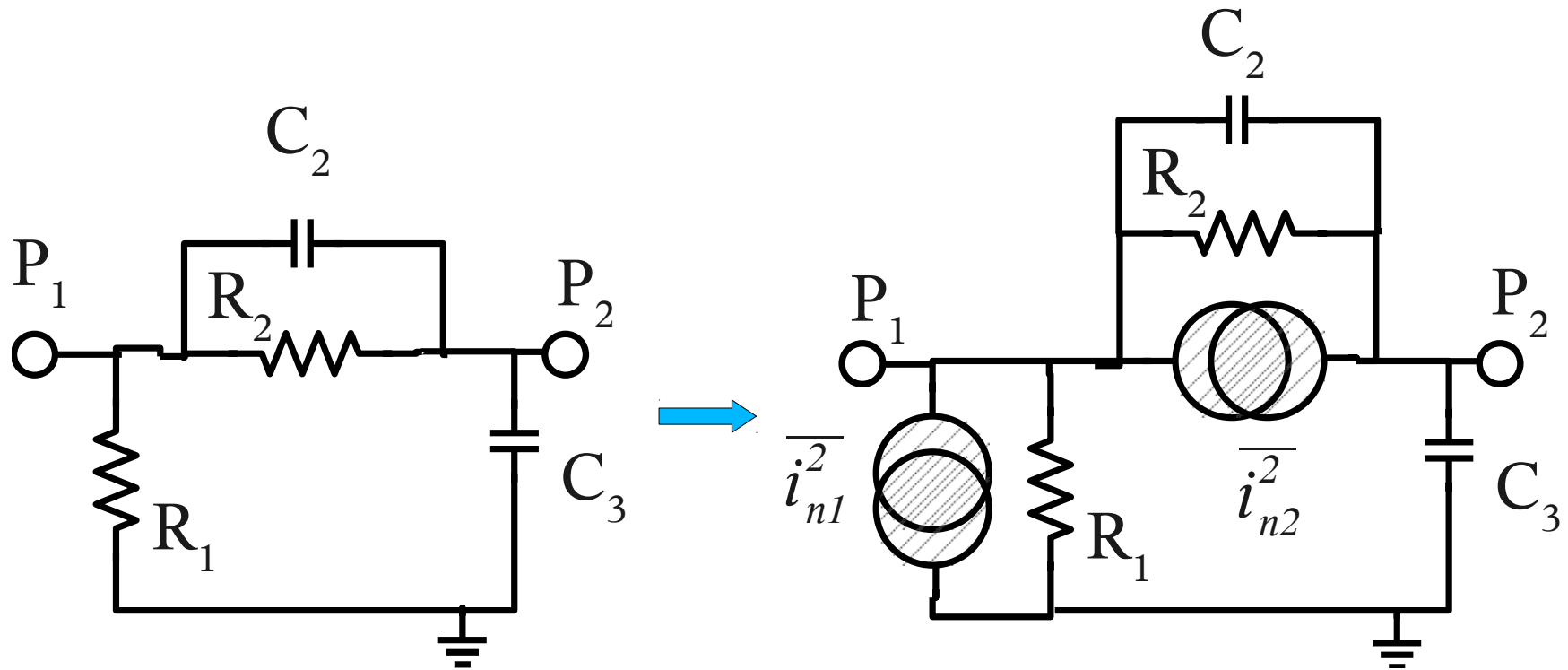
$$[C_s] = \frac{1}{4}([U] + [S])[C_y]([U] + [S])^+; \quad [C_s] = \frac{1}{4}([U] - [S])[C_z]([U] - [S])^+$$

$$Im(c_{nn}) = Im(\overline{v_{nn}^2}) = Im(\overline{i_{nn}^2}) = Im(\overline{b_{nn}^2}) = 0 \quad c_{ki} = c_{ik}^*$$

Method to form the noise admittance correlation matrix of an n -port

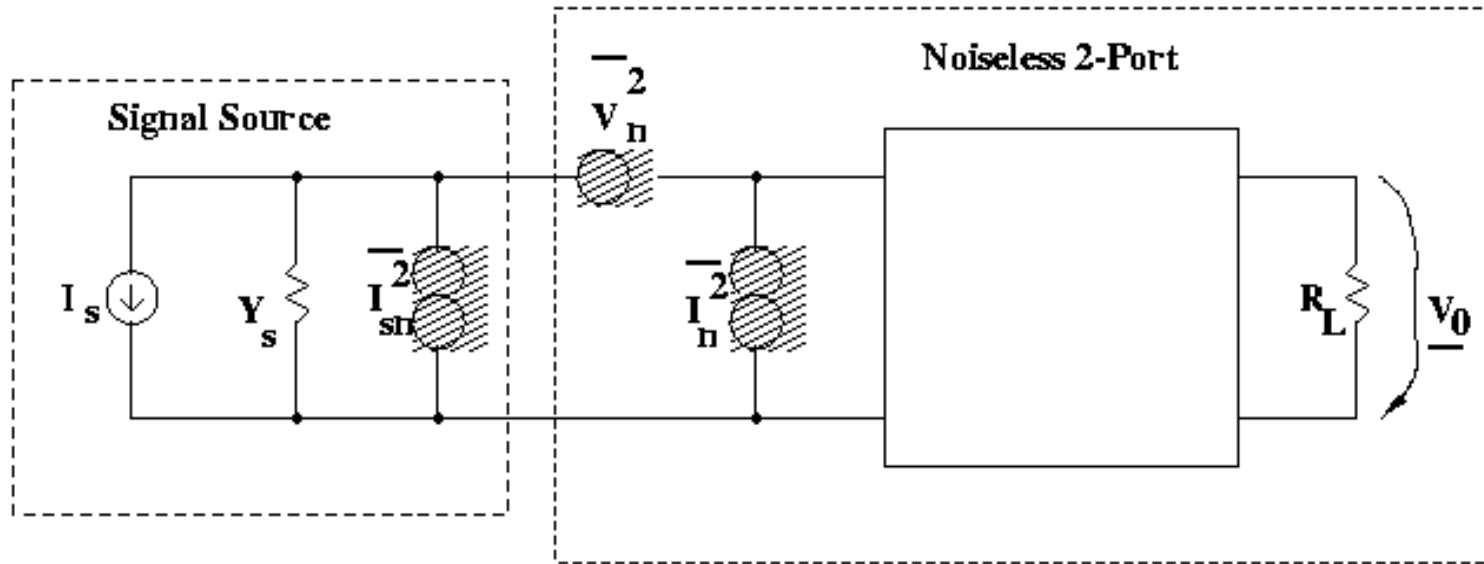
- $C_y[i,i]$ = sum of all noise currents connected to node i
- $C_y[i,j]$ = negative of sum of all noise currents between i and j
 - If $j = \text{GND}$, the noise current is only added to $C_y[i,i]$

Example:



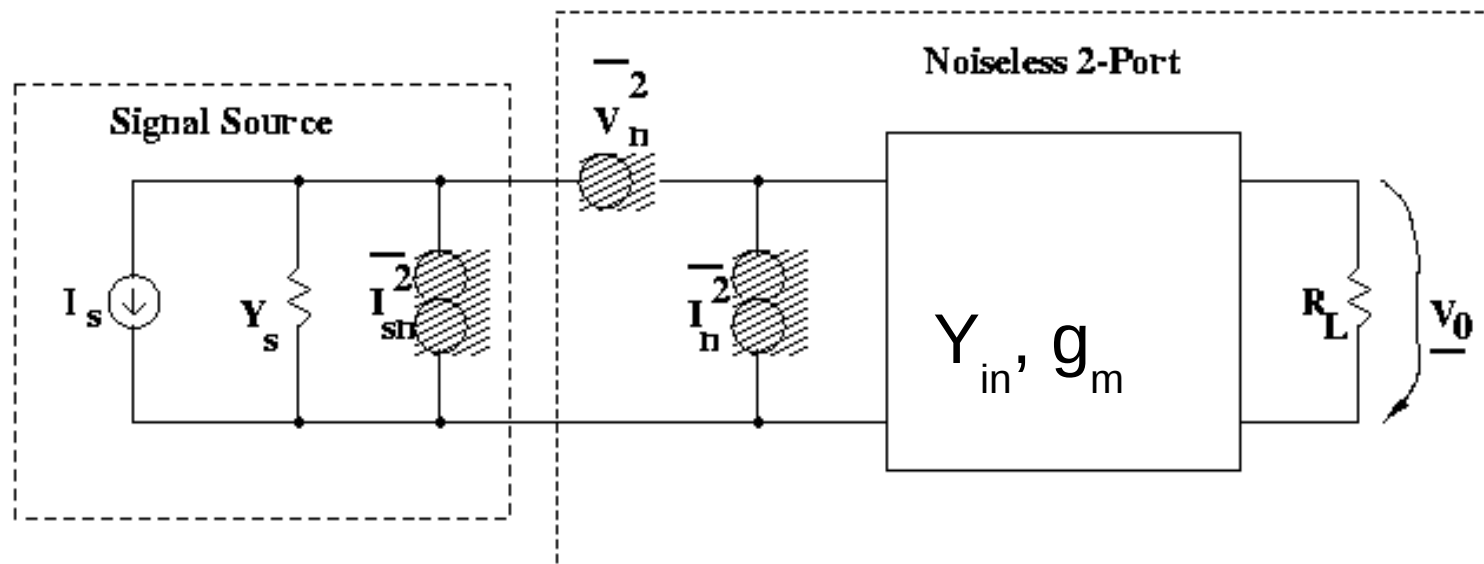
$$[C_Y] = \begin{bmatrix} \overline{i_{n1}^2} + \overline{i_{n2}^2} & -\overline{i_{n2}^2} \\ -\overline{i_{n2}^2} & \overline{i_{n2}^2} \end{bmatrix} = 4kT \Delta f \begin{bmatrix} G_1 + G_2 & -G_2 \\ -G_2 & G_2 \end{bmatrix}$$

Noise Factor of a 2-port driven by a signal source



- 2-port with input equivalent noise sources (sign is not important)
- Noise of signal source is typically thermal: $i_{sn}^2 = 4kT\Delta f \operatorname{Re}\{Y_s\}$
- Signal source may be a photodiode: $i_{sn}^2 = 4kT\Delta f G_{seq}$; $Y_s = j\omega C_D$
- G_{seq} is due to dark current and optical power.

Deriving the Noise Factor of the 2-Port



- Find input shortcircuit current i_{scn} due to i_{sn} , i_n , v_n by superposition
- Input short circuit current i_{scsn} due to i_{sn}
- Determine F as the ratio:
$$F = \frac{\overline{i_{scn}^2}}{\overline{i_{scsn}^2}}$$

Two-Port Noise Parameters (1)

Noise admittance formalism

$$v_n = v_n; i_n = i_u + i_c = i_u + Y_{\text{cor}} v_n$$

$$R_n = \frac{\overline{v_n^2}}{4kT \Delta f} \quad G_u = \frac{\overline{i_u^2}}{4kT \Delta f}$$

$$Y_{\text{cor}} = \frac{\overline{i_n v_n^x}}{\overline{v_n^2}} = G_{\text{cor}} + jB_{\text{cor}}$$

Noise resistance formalism

$$i_n = i_n; v_n = v_u + v_c = v_u + Z_{\text{cor}} i_n$$

$$R_u = \frac{\overline{v_u^2}}{4kT \Delta f} \quad G_n = \frac{\overline{i_n^2}}{4kT \Delta f}$$

$$Z_{\text{cor}} = \frac{\overline{v_n i_n^x}}{\overline{i_n^2}} = R_{\text{cor}} + jX_{\text{cor}}$$

Two-Port Noise Parameters (2)

$$F = 1 + \frac{\overline{v_n}^2 |Y_{cor} + Y_s|^2}{\overline{i_{sn}}^2} + \frac{\overline{i_u}^2}{\overline{i_{sn}}^2}$$

$$F = 1 + \frac{\overline{i_n}^2 |Z'_{cor} + Z_s|^2}{\overline{v_{sn}}^2} + \frac{\overline{v_u}^2}{\overline{v_{sn}}^2}$$

$$F = 1 + \frac{R_n}{G_s} |Y_{cor} + Y_s|^2 + \frac{G_u}{G_s}$$

$$F = 1 + \frac{G_n}{R_s} |Z_{cor} + Z_s|^2 + \frac{R_u}{R_s}$$

$$F = F_{MIN} + \frac{R_n}{G_s} |Y_s - Y_{sopt}|^2$$

$$F = F_{MIN} + \frac{G_n}{R_s} |Z_s - Z_{sopt}|^2$$

Constant Noise Circles on Smith Chart

Two-Port Noise Parameters (3)

$$Y_{\text{sop}} = G_{\text{sopt}} + jB_{\text{sopt}}$$

$$Z_{\text{sopt}} = R_{\text{sopt}} + jX_{\text{sopt}}$$

$$F_{\text{min}} = 1 + 2R_n(G_{\text{cor}} + G_{\text{sopt}})$$

$$F_{\text{min}} = 1 + 2G_n(R_{\text{cor}} + R_{\text{sopt}})$$

$$G_{\text{sopt}} = \sqrt{G_{\text{cor}}^2 + \frac{G_u}{R_n}}; B_{\text{sopt}} = -B_{\text{cor}}$$

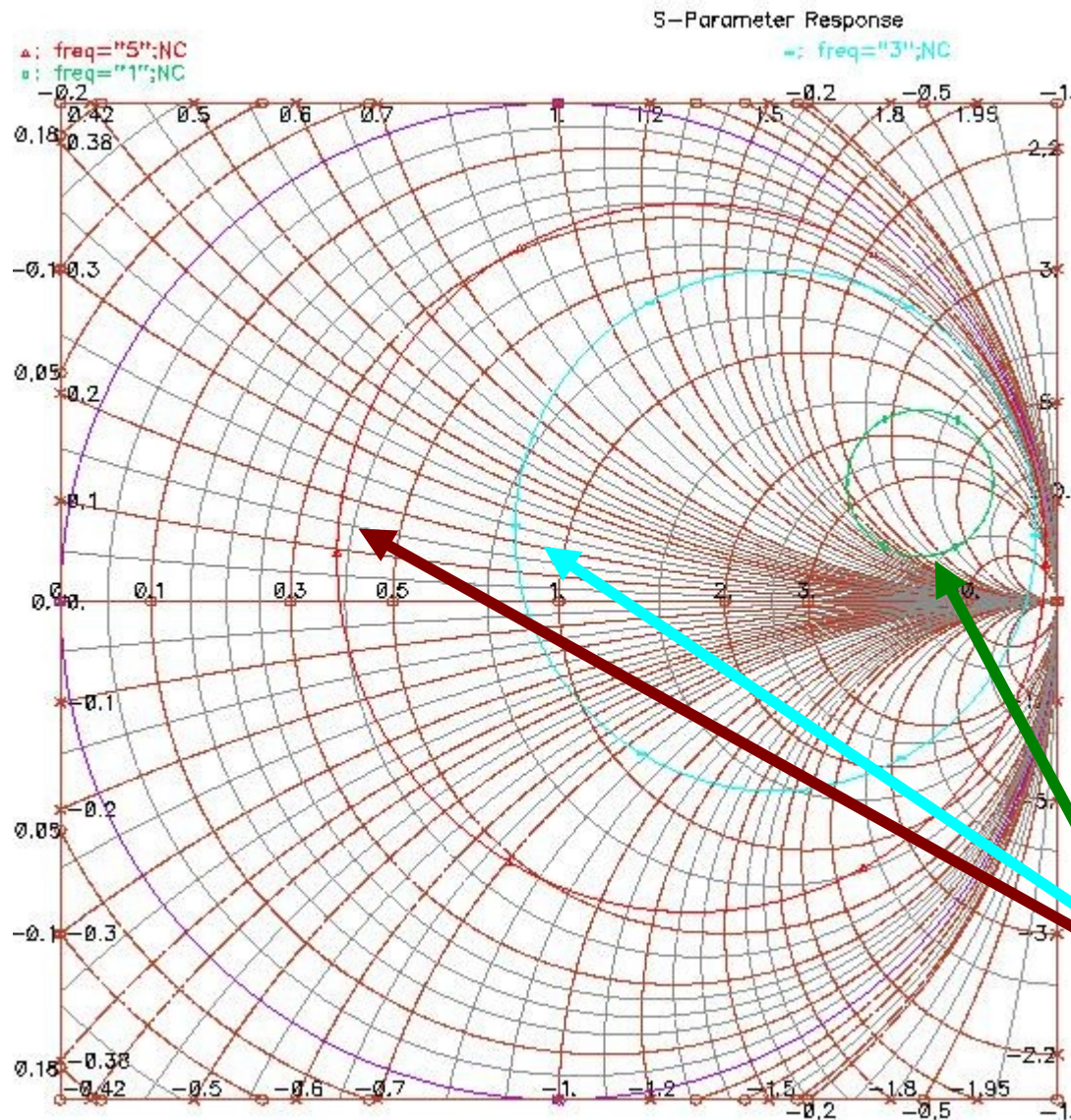
$$R_{\text{sopt}} = \sqrt{R_{\text{cor}}^2 + \frac{R_u}{G_n}}; X_{\text{sopt}} = -X_{\text{cor}}$$

$$Y_{\text{sop}} = \frac{1}{Z_{\text{sopt}}} \quad Y_{\text{cor}}^x = \frac{Z_{\text{cor}}}{|Z_{\text{sopt}}|^2}$$

$$R_n = G_n |Z_{\text{sopt}}|^2$$

$$G_u = \frac{R_u}{|Z_{\text{sopt}}|^2}$$

Two-Port Noise Circles



$$F(\Gamma_s) = F_{min} + 4 \frac{R_n}{Z_0} \frac{|\Gamma_s - \Gamma_{sopt}|^2}{(1 - |\Gamma_s|^2) |1 + \Gamma_{sopt}|^2}$$

$$r_i = \frac{\sqrt{N_i^2 + N_i(1 - |\Gamma_{sopt}|^2)}}{1 + N_i}$$

$$C_i = \frac{\Gamma_{sopt}}{1 + N_i}$$

$$N_i = \frac{F_i - F_{min}}{4 r_n} |1 + \Gamma_{sopt}|^2$$

**Constant Noise Circles
on Smith Chart**

Correlation Matrix and 2-Port Noise Parameters

$$[C_A] = \begin{bmatrix} \langle v_{n1} & v_{n1}^* \rangle & \langle v_{n1} & i_{n1}^* \rangle \\ \langle i_{n1} & v_{n1}^* \rangle & \langle i_{n1} & i_{n1}^* \rangle \end{bmatrix} = \begin{bmatrix} C_{uu^*} & C_{ui^*} \\ C_{iu^*} & C_{ii^*} \end{bmatrix} = \begin{bmatrix} R_n & \frac{F_{\text{MIN}} - 1}{2} - R_n Y_{\text{opt}}^* \\ \frac{F_{\text{MIN}} - 1}{2} - R_n Y_{\text{opt}} & R_n |Y_{\text{opt}}|^2 \end{bmatrix}$$

$$Y_{\text{opt}} = \sqrt{\frac{C_{ii^*}}{C_{uu^*}} - \left[\Re \left(\frac{C_{ui^*}}{C_{uu^*}} \right) \right]^2} + j \Re \left(\frac{C_{ui^*}}{C_{uu^*}} \right)$$

$$F_{\text{MIN}} = 1 + \frac{C_{ui^*} + C_{uu^*} Y_{\text{opt}}^*}{kT}$$

$$R_n = \frac{C_{uu^*}}{kT}$$

From Stephen Maas' "Noise"

Correlation Matrix and 2-Port Noise Parameters

$$[C_y] = \begin{bmatrix} \langle i_{n1} i_{n1}^* \rangle & \langle i_{n1} i_{n2}^* \rangle \\ \langle i_{n2} i_{n1}^* \rangle & \langle i_{n2} i_{n2}^* \rangle \end{bmatrix} = \begin{bmatrix} G_u + R_n |Y_{11} - Y_{cor}|^2 & R_n Y_{21}^* (Y_{11} - Y_{cor}) \\ R_n Y_{21} (Y_{11}^* - Y_{cor}^*) & R_n |Y_{21}|^2 \end{bmatrix}$$

$$R_n = \frac{C_{y22}}{|Y_{21}|^2} \quad Y_{cor} = Y_{11} - \frac{C_{y12}}{C_{y22}} Y_{21}$$

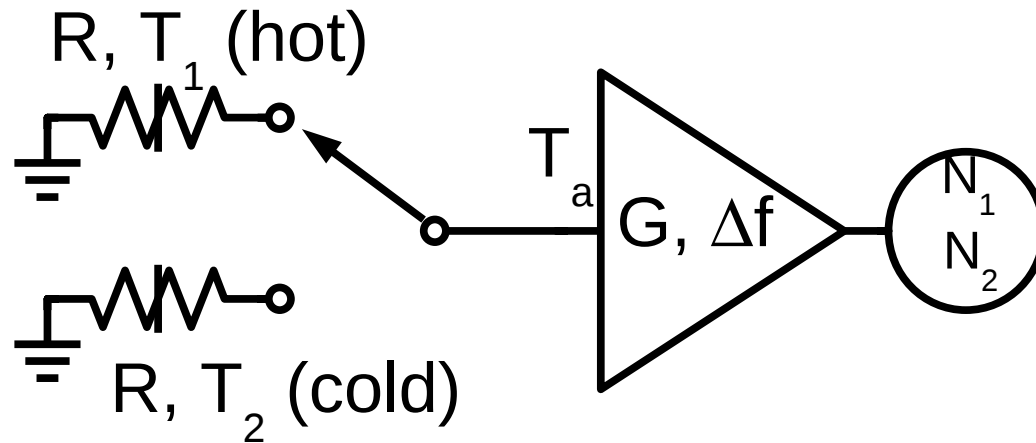
$$G_u = C_{y11} - R_n |Y_{11} - Y_{cor}|^2$$

From Stephen Maas' "Noise"

Noise in Passive 2-ports

- A lossless passive 2-port has $NF_{\text{MIN}} = 0$ dB
- In a lossy passive 2-port the noise figure is equal to the insertion loss.
- If a noisy 2-port is cascaded with a lossless passive 2-port the minimum noise figure is preserved.
 - Hence the popularity of reactive matching networks in tuned LNA design

Two-Port Noise Temperature Measurements



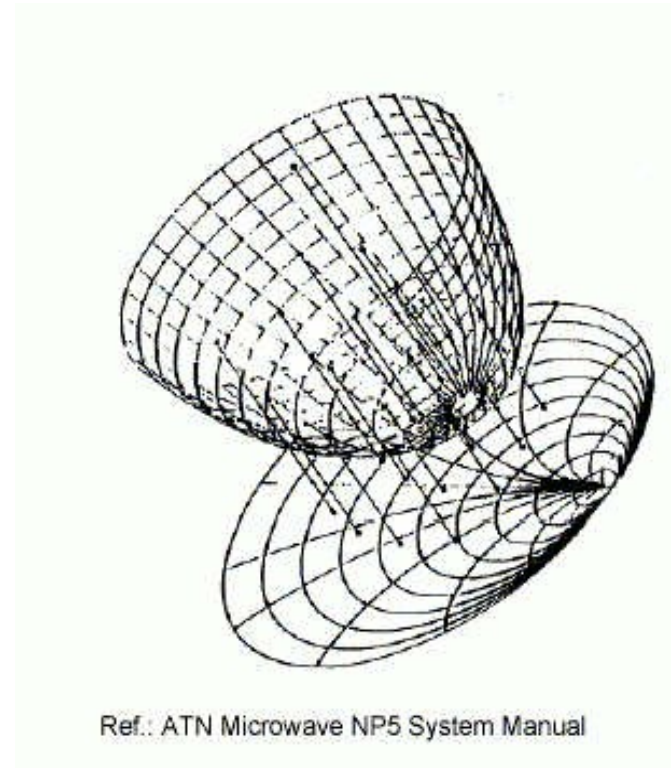
$$N_1 = GkT_1\Delta f + GkT_a\Delta f; \quad N_2 = GkT_2\Delta f + GkT_a\Delta f$$

$$Y = \frac{N_1}{N_2} = \frac{T_1 + T_a}{T_2 + T_a}; \quad T_a = \frac{T_1 - YT_2}{Y - 1}$$

- Also known as the *Y-factor* measurement
- Measures output noise for two loads at significantly different temperatures connected at the input of the two-port

Two-Port Noise Parameter Measurements

$$F_k = F_{\text{MIN}} + \frac{R_n}{G_{sk}} |Y_{sk} - Y_{\text{sopt}}|^2$$



- Want small R_n for insensitivity to source noise impedance mismatch

Two-Port Noise Parameter Measurements (2)

- The 4 noise parameters are measured indirectly using a Noise Figure Meter
- Measure noise figure for 4 or more different source impedances and solve for the noise parameters:

$$F_k = F_{\text{MIN}} + \frac{R_n}{G_{sk}} |Y_{sk} - Y_{\text{sopt}}|^2$$

$$k = 1..4..$$

- Choice of Y_{sk} is critical to meas. accuracy

Summary

- NF is a function of signal source impedance and of the 4 noise parameters of the 2-port
- For a 2-port there is an optimum signal source impedance which minimizes NF
- To achieve NF_{MIN} the 2-port must be "noise-matched"
- Noise matching can be achieved using negative feedback or (lossless) impedance transformation techniques
- The noise figure of a passive 2-port is equal to its insertion loss.